

METHOD FOR THE PREPARATION OF OLEFIN POLYMERISATION CATALYST
SUPPORT AND AN OLEFIN POLYMERISATION CATALYST

The present invention relates to a catalyst support, to a
5 preparation process thereof, to a Ziegler-Natta catalyst, as
well as to the use of the catalyst for polymerising olefins.

BACKGROUND ART

Ziegler-Natta (ZN) polyolefin catalysts are well known in the
10 field of polymers. Generally, they comprise (a) at least a
catalyst component formed from a transition metal compound of
Group 4 to 6 of the Periodic Table (IUPAC, Nomenclature of
Inorganic Chemistry, 1989), a metal compound of Group 1 to 3
of the Periodic Table (IUPAC), and, optionally, a compound of
15 group 13 of the Periodic Table (IUPAC) and/or an internal
donor compound. ZN catalyst may also comprise (b) further
catalyst component(s), such as a cocatalyst and/or an
external donor.

20 Various methods have been developed for preparing ZN
catalysts. In one method the catalyst components are
impregnated on a particulate support material, such as
silica, to obtain a solid ZN catalyst system. For example in
WO 01 55230 of Borealis a solution of a chlorine-containing
25 compound, e.g. ethylaluminium dichloride, and a magnesium
hydrocarbyloxy compound is first prepared and the obtained
solution is impregnated together with a transition metal
compound into a porous support.

30 Solid ZN catalysts, wherein no external support, such as
silica, is used, are also known in the field. US 4 496 660 of
Dow discloses a catalyst support formed by reacting in an
inert diluent (A) the reaction product of (1) an

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organomagnesium component, (2) an oxygen- and/or nitrogen-containing compound, optionally dissolved or dispersed to a halide containing compound of a transition metal; and (B) a transition metal-free halide source. In the examples the

5. compound (1) is combined with the compound (2) and a halogen-free aluminium compound and then a transition metal compound is added. The obtained solids are then reacted with the compound (B). EP 591 922 of Mitsui discloses a titanium catalyst prepared by contacting (A) a solution of a halogen-

10 containing magnesium compound, an alcohol having at least 6 carbon atoms and a hydrocarbon solvent, with an organoaluminum compound to form a solid complex which is treated with (B) a tetravalent titanium compound.

15 WO 99 55741 of Fina describes a process for preparing a Ziegler-Natta catalyst by (i) mixing in a hydrocarbon solvent a dialkyl magnesium compound with a chlorinating agent to precipitate a magnesium dichloride derivative. The chlorinating agent is obtainable from the reaction between an

20 alcohol ROH and an alkyl aluminium chloride. The precipitate is washed or reacted to remove unwanted reducing species and the obtained magnesium dichloride derivative is titanated. WO 99 58584 of Borealis describes a further method for preparing a ZN catalyst, wherein a Mg compound is first reacted with an

25 alcohol and the obtained complex is added to a solution of chlorine containing aluminium compound to form a solid reaction product. The obtained slurry is used as such in the next step and to this slurry titanium tetrachloride is added. EP 197 166 of Dow describes a catalyst solution, wherein (A)

30 an organomagnesium compound, (B) an organic OH-containing compound, (C) a reducing halide source of Al or B and (D) a transition metal compound are added in the order (A), (B), (C) and (D); or (A), (B), (D) and (C), and the obtained

reaction solution is used as such for the polymerisation. Again no washing steps between the additions are made and no separation of the final reaction product from the reaction media is effected.

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Accordingly, although much development work has been done in the field of Ziegler-Natta catalysts, there remains a continuing search for alternative or improved methods of producing ZN catalysts with desirable properties, such as morphology.

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SUMMARY OF THE INVENTION

The present invention provides a further process for preparing a solid catalyst support, and a ZN catalyst component based on said support, with an unexpected effect. A further solid catalyst support and a further ZN catalyst component with improved properties are also provided.

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A further aspect of the invention is to provide an olefin polymerisation process using the ZN catalyst prepared according to the preparation process of the invention.

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DESCRIPTION OF THE INVENTION

It has surprisingly been found that when a solid reaction product is formed from a magnesium hydrocarbyloxy compound and a halogen-containing compound of an element of Group 13 or 14 of the Periodic Table (IUPAC, Nomenclature of Inorganic Chemistry, 1989, used also below), and the obtained solid product is recovered from the reaction mixture, a solid catalyst precursor, herein referred as a catalyst support material, with i.a. markedly improved morphology can be obtained. The support material of the invention can then be treated with further catalytically active compound(s), such

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as with one or more transition metal compounds, to obtain a catalyst component for olefin polymerisation.

Due to the beneficial properties of the support material of the invention, the good morphology is maintained during the treatment step of the support with further catalytically active compounds, whereby also the resulting final catalyst component has an excellent morphology, such as a desirable particle size and a narrow particle size distribution (PSD).

Furthermore, the final catalyst of the invention exhibits high catalytic activity and the polymer product produced therewith has i.a. a decreased amount of fines (i.e. particles with size $< 100 \mu\text{m}$), i.e. below 15 %, preferably below 10 % of fines. Even fines content below 6 % can be obtained.

According to the method of the invention a particulate catalyst support to be used as a polymerisation catalyst component is prepared first by (a) contacting a solution of a magnesium hydrocarbyloxy compound (compound (1)) with (b) a solution of a halogen-containing compound of an element of Group 13 or 14 of the Periodic Table (IUPAC) (compound (2)) to obtain a solid particulate reaction product. Then the obtained reaction product is recovered from the reaction mixture by separating the solid product from the liquid reaction medium and/or by washing the product before it is used as a support material.

In a preferred embodiment of the invention the solution of the compound(s) (1) is added to the solution of compound(s) (2) to cause the solidification (precipitation) of the solid reaction product. A slowly addition under mixing is

preferred. By slowly addition it is meant herein that the solution (1) is added gradually, e.g. dropwise or other similar means, to cause a uniform solidification reaction as known in the art. The solidification step may be effected
5 suitably at the ambient temperature.

It has been found that in order to achieve the beneficial properties of the support material, the obtained solid reaction product should be recovered from the reaction
10 mixture of solution (1) and (2) before the use as a support. The recovery step can be effected in various ways including the separation of the liquid reaction medium from the solid reaction product, e.g. by filtration, decantation or suction, and/or washing the solid product with a wash solution e.g. in
15 a manner known in the art, before it is used as a support material. Thus the possible washing step can be carrier out after the solids are separated from the liquid medium or, alternatively, without any separation of the solids from the reaction mixture (or the liquid reaction medium is removed
20 only partially), by adding the wash solution directly to the reaction mixture. The recovery step of the invention covers also the dilution of the reaction mixture and the use of the diluted support slurry in the next step for preparing the catalyst component.

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It is evident for a skilled person that the washing efficiency can be varied within the scope of the invention depending on the desired washing effect and can be controlled e.g. by the number of the washing steps, the temperature, the
30 solvent(s) used for washing, the amount of the wash solution and the washing time. The wash temperature can be e.g. 0 - 100 °C, suitably 20 - 100 °C, e.g. 40 - 80 °C, such as 55 - 70 °C. Thus the duration of a washing (e.g. the mixing time of

the slurry in a wash solution) depends on the desired effect and can be chosen accordingly.

Further treatment steps of the solid reaction product may also be possible after the combination of solutions (1) and (2) before or during the recovery step of the invention. Such treatment includes e.g. a heating step of the reaction mixture after the solidification at an elevated temperature, e.g. up to 100 °C, such as 40 to 80 °C, suitably 50 to 75 °C, for a suitable period of time, such as from 5 minutes to 24 hours, e.g. 10 to 120 minutes, such as 20 to 60 minutes, before the recovery step.

In a preferable embodiment, the molar ratio of the element of Group 13 or 14 of the Periodic Table to magnesium in the catalyst support material of the invention is at least 0.3 (≥ 0.3). Preferably the molar ratio of said element of Group 13 or 14 of the Periodic Table to magnesium is at least 0.4 (≥ 0.4), or preferably at least 0.5 (≥ 0.5), or at least of 0.6 (≥ 0.6). Said ratios result in catalyst with very good morphology and reduced amount of fines content of the produced polymer product. In a further embodiment of the invention said molar ratio may be even at least 0.7 (≥ 0.7) or 0.80 (≥ 0.80), such as 0.85 (≥ 0.85), depending on the properties desired for the catalyst. In principle, the upper limit of said ratio range is not limited, but may be e.g. 1.1. In one preferred embodiment said upper limit of said molar ratio is 0.99. The above-said molar ratio can be determined in a known manner, e.g. using flame atomic absorption method with e.g. a nitrous oxide/acetylene flame.

Accordingly, the recovery step already improves i.a. the morphology of the catalyst and the produced polymer compared

to the prior art practices, wherein the reaction product has not been recovered (i.e. the reaction mixture is used as such or the solids are separated from the reaction media and used without any washing step). And said preferable molar ratio of the support material can provide further advantages, such as a preferred morphology with e.g. desirable yields of the catalyst component.

It is generally known that the said molar ratio of the obtained catalyst support can depend on the used starting material, the used preparation method of the support material, reaction conditions and any treatment steps of the reaction product after the combination of the solutions (1) and (2), and can be chosen accordingly to achieve the desired ratio.

Preferably, the molar ratio of the element of compound (2) to magnesium in the support material is adjusted to a desired range by means of the recovery step of the invention, i.e. by separating the solids from the liquid reaction medium and/or by washing the solids as described above. Particularly, the obtained solid reaction product is washed with a wash solution, and the washing procedure can be repeated, if needed, until the desired ratio is obtained. The ratio can be monitored between the washings, if needed, e.g. by analysing the support samples in a conventional manner the relevant contents of the reaction product or the reaction medium, e.g. the mol-% of Mg and the mol-% of the element from Group 13 or 14 of the Periodic Table in the formed carrier material.

Suitably, a moderate washing is effected to achieve the molar ratio of the invention. Thus the washing treatment of the invention provides convenient means for adjusting the ratio

of the support elements to the preferred level (generally, the more thorough washing the lower ratio is obtained).

The said molar ratio of the support material of the invention
5 is believed to give a beneficial loading of the active species in the final catalyst component.

After the recovery step of the invention, the solid reaction
product can be used as a support material for further
10 catalytically active compounds, such as one or more transition metal compound(s) to form a final polymerisation catalyst component, such as the ZN catalyst component of the invention. The term "particulate/solid support material" means herein an intermediate, i.e. catalyst precursor, that
15 is treated with further catalyst forming compounds as defined below to obtain the final catalyst component. Preferably, the solid support of the invention is first formed in the absence of the catalyst forming transition metal compound, and after the formation thereof treated with said transition metal
20 compound.

Accordingly, in the method of the invention for preparing a Ziegler-Natta catalyst component, the catalyst support of the invention, preferably prepared according to the present
25 method, is suspended in an organic solvent and treated at least with one transition metal compound. The treatment step is preferably effected in a manner known in the art.

Generally, in the final solid catalyst particles, the molar
30 ratio of Mg:Ti can be e.g. between 10:1 to 1:10, preferably less than 5:1, such as between (less than 5:1) and 1:1. The molar ratio of Ti:Al can be e.g. between 10:1 to 1:2, e.g.

3:1 to 1:1. The ratios can be determined in a manner known in the art.

The final catalyst component, e.g. the ZN catalyst component, thus obtained may be combined with further catalyst component(s) conventionally used in the art, such as a cocatalyst (e.g. aluminium alkyl compounds) and/or an external donor compound selected from silanes and (internal) electron donors as defined below. Said further catalyst component(s) can be combined with the present catalyst component during the preparation method of the present catalyst component, or during the actual polymerisation step by adding the catalyst component of the invention and the further component(s) separately into a reactor.

The invention thus provides a controllable method to obtain active catalyst particles with i.a. the desirable loading of the active species and highly preferable morphology, e.g. a narrow particle size distribution and markedly reduced fines content in the polymer. The catalyst support and the final catalyst prepared thereof are also novel with improved properties and thus form part of the invention.

Depending on the chosen reaction conditions, the average size of the catalyst particles of the invention may vary between 1 to 500 μm , e.g. 5 to 500 μm , advantageously 5 to 200 μm or 10 to 150 μm . Even an average size between 5 to 50 μm , such as 10 to 20 μm is possible. The usable particle size depends on the polymerisation wherein the catalyst is used.

In a still further embodiment of the invention the catalyst component(s) can be prepolymerised before the actual polymerisation step.

Starting Compounds for the Support Material

The basic idea of the invention lies in the specific post treatment step of a reaction product formed from the Mg and the Group 13 or 14 compound, which brings the advantages of the invention. Thus the starting material for the catalyst support of the invention can be chosen from one or more magnesium compound(s), provided that at least one Mg compound contains hydrocarbyloxy, and from one or more halogen-containing compound(s) of an element of Group 13 or 14 of the Periodic Table, which are usable for forming a ZN catalyst and which can be brought in a solution and, when contacted together in suitable conditions, form a reaction product which solidifies in said reaction media. Such compounds, the solutions thereof, as well as the reaction conditions to obtain the solid reaction product thereof, are within the skills of a person working in the field of Ziegler-Natta chemistry..

Accordingly, the catalyst support of the invention comprises a reaction product formed at least from:

1) Compound (1): A magnesium hydrocarbyloxy compound of a general formula (I):

$$\text{Mg}(\text{OR}_1)_{2-n}(\text{R}_1)_n\text{X}_x \quad (\text{I}),$$

wherein each R_1 is independently a C_{1-20} hydrocarbyl group, e.g. a C_{2-15} group, preferably a C_{3-10} group, such as a C_{4-10} group, suitably a C_{4-10} group e.g. an alkyl, cycloalkyl, alkylcycloalkyl, cycloalkylalkyl, aryl, arylalkyl, or alkylaryl, wherein "alkyl" used as alone or as part of another option can be linear or branched and "aryl" is preferably of 5-12 carbon ring atoms, suitably phenyl or naphthyl; e.g. each R_1 is independently an ethyl, propyl,

butyl, pentyl, hexyl, heptyl, octyl; each X is independently a halogen, preferably chlorine; $0 \leq n < 2$ and n may or may not be an integer; $0 \leq x < 2$ and may or may not be an integer; and the sum of $(2-n)$, n and x is 2.

- 5 In a preferred embodiment of the invention, a magnesium hydrocarbyloxy compound of formula $Mg(OR_1)_{2-n}(R_1)_nX_x$ (I), wherein each R_1 and X are independently as defined above; x is 0 and $0 \leq n < 2$, is used, which may be commercially available or, preferably, is a reaction mixture of a
- 10 magnesium alkyl compound of formula $Mg(R_1)_2$ (III), wherein each R_1 independently is as defined above, with an alcohol R_1OH , wherein R_1 is as defined above;

and

- 15 2) Compound (2): A halogen-containing compound of an element of Group 13 or 14 of Periodic Table (IUPAC), which is preferably a compound of Group 13, such as a halogen-containing aluminium or boron compound. Halogen is e.g. chlorine, bromine or iodine, preferably chlorine. In one
- 20 preferred embodiment said compound is of formula (II):
 $Al(R_1)_xX_{3-x}$ (II),
wherein each R_1 is independently as defined above in formula (I), and particularly in case of formula (II) an alkyl of up to 6, such as up to 4, carbon atoms; and each
- 25 X is independently a halogen, such as chlorine; $0 \leq x < 3$ and x may or may not be an integer; e.g. dialkyl aluminium chloride, such as dimethyl aluminium chloride, diethyl aluminium chloride, diisobutyl aluminium chloride, or alkyl aluminium dichloride, such as ethyl aluminium
- 30 dichloride (EADC) or methyl aluminium dichloride; ...

The molar ratio of the element of compound (2) to Mg used may be between 0.5:1 and 2:1, preferably 0.8:1 to 1.2:1, such as 1:1.

5 Optionally, the present support material comprises further catalytically active compounds, e.g. those useful in a ZN catalyst, such as one or more (internal) electron donors, e.g. those known in the art for (co)polymerising propylene and higher olefins, including organic compounds containing
10 oxygen, nitrogen, sulphur and/or phosphorus, such as organic acids, organic acid anhydrides, organic acid esters, alcohols, ethers, aldehydes, ketones, amines, amine oxides, amides, thiols, various phosphorus acid esters and amides, and the like, added as such or formed in situ, and such
15 compound(s) may be added into one of the solutions of (1) and (2) before the combination of the solutions, or into the reaction media of compounds (1) and (2). Preferably, the support consists of the reaction product of compound (1), optionally prepared from compound (III) and R_1OH as defined
20 above, and of compound (2).

Alternatively, said at least one (internal) electron donor or further compound(s) can be added after the formation of the support product, e.g. when treating the obtained support with
25 the transition metal compound.

Solutions of the Starting Compounds

The term "solution" is understood herein broadly to include solutions prepared from (a) one or more of the support
- 30 - forming compounds in liquid form (liquid at the room temperature or a melt prepared at a higher temperature), and/or (b) from an organic solvent(s).

The solutions are suitably formed using an organic solvent that dissolves the compounds. Preferred solvents include inert hydrocarbons, e.g. linear or branched aliphatic, alicyclic or aromatic C₅₋₂₀ hydrocarbons, preferably C₆₋₁₂ hydrocarbons, wherein the ring systems may contain hydrocarbon, e.g. C₁₋₆ alkyl substituents, such as cyclohexane, hexane, heptane, octane or toluene, or any mixtures thereof. E.g. linear or branched alkanes, e.g. hexane, heptane or octane, may be used.

Wash Solution

As the wash solution, e.g. any organic solvent or mixtures thereof known in the art can be used. Preferable solvents include hydrocarbons as defined above, e.g. pentane, hexane or heptane, particularly heptane.

The Catalyst Component for the Polymerisation of Olefins

The invention further provides a catalyst component, comprising the catalyst support of the invention treated with one or more further catalytically active compound(s), such as one or more transition metal compound(s), e.g. those conventionally used in the ZN catalysts, metallocenes, metallocene type complexes, chromium compounds etc., or any mixtures thereof, and/or a cocatalyst.

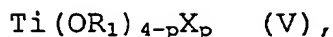
Preferably a Ziegler-Natta catalyst component is provided, wherein said support is treated at least with:

- 3) One transition metal compound of Group 4 to 10, preferably of Group 4 to 6, more preferably of Group 4, of the

Periodic Table (IUPAC). The transition metal compound is suitably a Ti compound. Particularly, a tetravalent Ti compound can be used. Examples of such compounds are:



wherein each X is independently defined as above in formula (I), such as Cl; and



5 wherein each X and R_1 are as defined above in formula (I)
p is 0, 1, 2 or 3;

Preferably, titanium tetrachloride is used.

In the method of the invention for preparing a catalyst
10 component, the solid catalyst support of the invention,
preferably as prepared by the present method, is treated with
a further catalytically active compound(s) as defined above.
Preferably a Ziegler-Natta catalyst component is prepared by
suspending the particulate support of the invention in an
15 organic solvent as defined above and treating the support at
least with one transition metal compound as defined above.
The treatment step is preferably effected in a manner known
in the field of ZN chemistry. The molar ratio of the
transition metal to be added is preferably 2 to 0.3, e.g. 1.5
20 to 0.4, such as 1 to 0.5 to one mol Mg present in the support
material.

In case of a ZN catalyst, the optional addition of an
(internal) electron donor can be effected, as said above,
25 during the formation of the support or, alternatively after
the formation of the support product, e.g. together with the
transition metal compound.

Embodiments

30 The solution of the magnesium hydrocarbyloxy compound is
preferably a solution of a magnesium alkoxy compound which
may be a commercially available magnesium alkoxy compound or
be prepared from a magnesium alkyl compound and an alcohol.

Accordingly, in a preferred embodiment for preparing the catalyst support and a supported polymerisation catalyst, suitably a ZN catalyst component, of the invention:

- 5 A solution (1) containing a magnesium hydrocarbyloxy compound of formula $Mg(OR_1)_{2-n}(R_1)_nX_x$ (I), wherein R_1 and X are as defined above; x is 0 and $0 \leq n < 2$, is prepared first:

by contacting, in a hydrocarbon solvent (e.g. heptane), a compound of formula $Mg(R_1)_2$ (III), wherein R_1 is as defined
10 above under formula (I), e.g. each R_1 is independently methyl, ethyl, propyl, butyl, pentyl, hexyl, heptyl or octyl, e.g. di(n-butyl) magnesium, n-butyl sec-butyl magnesium, butyl ethyl magnesium or butyl octyl magnesium, preferably butyl octyl magnesium (BOMAG);

- 15 with an alcohol of formula R_1OH , wherein R_1 is as defined above under formula (I), suitably a cycloalkyl, cycloalkylalkyl, aryl, alkylaryl, arylalkyl or alkyl, each containing from 2 to 15, preferably from 3 to 10 carbon atoms. Preferably R_1 is a C_{3-15} cycloalkyl or branched or
20 unbranched C_{3-15} alkyl, preferably a C_{4-10} cycloalkyl or a branched or unbranched C_{4-10} alkyl, such as cyclopentanol, 2-methyl-2-propanol, 2-ethyl-1-butanol, 2-methyl-1-pentanol, 2-ethyl-pentanol, 2-ethyl-1-hexanol, n-heptanol, n-octanol and decanol, preferably 2-ethyl-1-hexanol. The alcohols which are
25 usable to transform the magnesium hydrocarbyl to a magnesium hydrocarbyloxy complex soluble in a hydrocarbon solvent, are known in the art or can be readily determined by a skilled person. Said contact is effected in a temperature between 0 and 100 °C, preferably at 10 - 40 °C, e.g. at 20 - 30 °C. The
30 reaction can be completed by heating the system at 50 - 100 °C for 10 to 100 min. Preferably the alcohol is added to the Mg solution. The molar ratio of Mg dihydrocarbyl to R_1OH

(Mg:R₁OH) is preferably from 1:1 to 1:4, more preferably 1:1 to 1:3.5, e.g. 1:1.5 to 1:3.5, especially 1:1.8 to 1:3.1.

The solution (2) of the halogen-containing compound is prepared by dissolving in a hydrocarbon solvent as defined above (e.g. toluene) a compound of formula



wherein each R₁ is independently as defined above, preferably an alkyl of up to 6, such as up to 4, carbon atoms; and each X is independently a halogen, such as chlorine; and x may or may not be an integer $0 \leq x < 3$; e.g. dimethyl aluminium chloride, diethyl aluminium chloride, diisobutyl aluminium chloride, ethyl aluminium dichloride and methyl aluminium dichloride, preferably ethyl aluminium dichloride (EADC). Such solutions may also be commercially available, whereby they may be further diluted, if desired, with a solvent as defined above.

The prepared reaction mixture (1), i.e. Mg-hydrocarbyloxy-containing solution (1), is then added slowly to the obtained Al solution (2).

The addition may be effected under stirring suitably at room temperature. After the addition the formed slurry may be heated to e.g. 20 to 100 °C, such as 40 to 80 °C, suitably 50 to 70 °C, for a suitable period of time, such as from 5 minutes to 24 hours, e.g. 10 to 120 minutes, such as 30 to 60 minutes.

In case of EADC, the molar ratio of Al:Mg used may be of 0.5:1 to 2:1, preferably 0.7:1 to 1.5:1, or 0.8:1 to 1.2:1,

such as 0.9:1 to 1.1:1, suitably 1:1. If another Al compound is used in place of EADC, then the Al compound is used in an amount that results in a halogen content which corresponds to the halogen content obtained with EADC at the above given ratios.

The formed reaction product is washed with heptane until a molar ratio of Al:Mg of ≥ 0.3 , e.g. of ≥ 0.4 suitably of ≥ 0.6 , preferably $0.4 \leq \text{Al:Mg} \leq 1.1$, such as $0.6 \leq \text{Al:Mg} \leq 0.99$, or e.g. $0.7 \leq \text{Al:Mg} \leq 0.99$ is achieved. In one further embodiment also a ratio of ≥ 0.80 , e.g. ≥ 0.85 , such as $0.85 \leq \text{Al:Mg} \leq (0.99 \text{ to } 1, \text{ e.g. } 0.99)$ may be used. The washing step can be carried out in a temperature between 0 - 100 °C, suitably 20 - 100 °C, e.g. 40 - 80 °C, such as 55 - 70 °C.

The solid catalyst support obtained can then be used for the preparation of the catalyst component. Preferably, the support is slurried in a fresh hydrocarbon solvent as defined above (e.g. heptane) and to the slurry titanium tetrachloride is added slowly e.g. in a manner known in the art, at the temperature of 0 - 100 °C, preferably at 10 - 50 °C. The components are allowed to react with each other e.g. at 20 - 100 °C, e.g. 50 - 80 °C, for 10 - 120 minutes, such as 30 - 60 minutes. Titanium tetrachloride is added to the support material e.g. in a molar ratio of 2 to 0.3 mol Ti, preferably 1 to 0.5 mol Ti, to one mol of Mg in the support.

The supported catalyst particles may then be washed and dried in a conventional manner.

In a still further embodiment of the method of the invention, a solution of the halogen-containing compound of Group 13 or

14 of the Periodic Table (compound (2)), preferably an Al-Cl compound of formula (II) as defined above, is dispersed as droplets to an inert immiscible solvent to form an emulsion.

- 5 The solvent of the continuous phase is preferably a highly fluorinated hydrocarbon solvent (i.e. the majority of the -C-H units are replaced with -C-F units) or a perfluorinated hydrocarbon solvent (i.e. all -C-H units are replaced with -C-F units), which optionally contain functional groups (See
10 the articles of A. Enders and G. Maas in "Chemie in unserer Zeit", 34. Jahrg. 2000, Nr.6, and of Pierandrea Lo Nostro in "Advances in Colloid and Interface Science, 56 (1995) 245-287, Elsevier Science). Said fluorinated solvent is preferably a perfluorinated hydrocarbon (e.g. perfluorinated
15 alkane, such as perfluorohexane, perfluoroheptane, perfluorooctane, perfluorononane or perfluorodecane, preferably perfluorooctane).

To the obtained emulsion, a solution of the Mg compound (1),
20 preferably a reaction mixture of R_1OH and a magnesium dialkyl compound (III) as defined above, in an organic solvent, e.g. inert hydrocarbon as defined above, such as heptane, is added (preferably slowly) to cause the solidification of the reaction product.

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The similar addition temperatures and subsequent heat treatment of the reaction slurry as described under "Embodiments" above may be used. After the formation of the solid reaction product, the solvents of the system, i.e. the
30... solvent(s) used for the starting compounds together with the solvent of the continuous phase, are removed and the solid product is washed using a wash solvent and the wash temperature as described under "Embodiments" above.

Preferably, the washing is carried out with heptane at elevated temperature to achieve the support material of the invention. Preferably, the molar ratio of the element of compound (2) (e.g. Al):Mg of the support material is adjusted
5 with the washing step to the level of the invention.

This embodiment provides a convenient alternative for moderate washing of the product to achieve said ratios in higher levels, e.g. between 0.6 and 0.99, such as 0.70 to
10 0.85, with, again, e.g. an excellent morphology of the obtained catalyst and the resulting polymer product.

Polymerisation Process

As mentioned above the catalyst particles of the invention
15 can be used as such or together with a separate cocatalyst and/or an electron donor, as a Ziegler-Natta catalyst for the (co)polymerisation of an olefin in a manner known in the art. It is also possible to combine said catalyst with one or more other ZN and/or non-ZN catalysts.

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The olefin to be polymerised using the catalyst system of the invention can be any olefin polymerisable in a coordination polymerisation including an alpha-olefin alone or a mixture of one or more comonomers. Preferable olefins are alpha-
25 olefins, e.g. ethylene or propene, or a mixture of ethylene or propene with one or more alpha-olefin(s). Preferable comonomers are C2-C12 olefins, preferably C4-C10 olefins, such as 1-butene, isobutene, 1-pentene, 1-hexene, 4-methyl-1-pentene, 1-heptene, 1-octene, 1-nonene, 1-decene, as well as
30 diene, such as butadiene, 1,7-octadiene and 1,4-hexadiene, or cyclic olefins, such as norbornene, and any mixtures thereof.

The present catalyst is particularly preferred for the polymerisation of polyethylene and any copolymers thereof. It may also suitably be used to produce e.g. polypropylene homopolymers and any copolymers thereof.

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Polymerisation may be effected in one or more, e.g. one, two or three polymerisation reactors, using conventional polymerisation techniques, in particular gas phase, solution phase, slurry or bulk polymerisation. Polymerisation can be a
10 batch or continuous polymerisation process. Generally a combination of slurry (or bulk) and at least one gas phase reactor is preferred, particularly with gas phase operation coming last.

15 For slurry reactors, the reaction temperature will generally be in the range of 40 to 110 °C (e.g. 60 - 110 °C), the reactor pressure will generally be in the range 5 to 80 bar (e.g. 50-60 bar), and the residence time will generally be in the range 0.3 to 5 hours (e.g. 0.5 to 2 hours). The diluent
20 used will generally be an aliphatic hydrocarbon having a boiling point in the range -70 to +100 °C. In such reactors, polymerisation may, if desired, be effected under supercritical conditions.

25 For gas phase reactors, the reaction temperature used will generally be in the range 60 to 115 °C (e.g. 70 to 110 °C), the reactor pressure will generally be in the range 10 to 25 bar, and the residence time will generally be 1 to 8 hours.

30 ---Generally the quantity of catalyst used will depend upon the nature of the catalyst, the reactor types and conditions and the properties desired for the polymer product. Conventional

catalyst quantities, such as described in the publications referred herein, may be used.

With the method of the invention a catalyst system with a
5 high bulk density and a good morphology is obtained and the catalyst exhibits a high catalytic activity. According to the so-called "replica effect" the bulk density and the morphology correlates with product bulk density and product morphology.. Thus the catalyst leads to a polymer which also
10 has advantageous properties, e.g. low fines level.

EXAMPLES

The following examples are provided by way of illustration of the invention. All the used starting materials and solvents
15 are commercially available or can be prepared according or analogously to methods described in the literature, e.g.:
(C_4H_9)_{1.5}Mg(C_8H_{17})_{0.5} in 20 wt-% heptane solution: supplied by Crompton, Germany (BOMAG); $EtAlCl_2$ in 18.5 wt-% toluene solution: Crompton, Germany (EADC); triethylaluminium in 20
20 wt-% heptane solution (TEA-20): Crompton, Germany; $TiCl_4$: Aldrich, Germany; octadecafluorooctane (PFO): P&M Scientific Industrial Association, Russia.

The particle size distribution was analysed by Coulter in a manner known in the art.

Examples 1 to 3

The effect of the wash to the molar ratio of the support is shown with examples 1 to 3.

The wash efficiency was changed in the carrier preparation by
30 -- changing the mixing speed in the wash, and by changing the number of wash cycles of the carrier material. First, the mixing speed was decreased in the heptane wash of the precipitated carrier material from 200 rpm to 100 rpm to

decrease the wash efficiency (example 2). Secondly, the number of heptane washes of the support material was decreased from two to one (example 3), also in order to decrease the wash efficiency. The changes are listed in Table

5 1.

Table 1. The changes in the carrier preparation recipe in Examples 1 - 3

Examples	1	2	3
Mixing speed in C ₇ wash (rpm)	200	100	200
Number of heptane washes	2	2	1

10 **Preparation of the catalysts:**

The carrier and the catalyst synthesis were done in a 20 l reactor. Strictly inert conditions were used in all the experiments.

15 **Addition of PFO:**

6.9 l (12.2 kg, 27.8 mol) of PFO was added to the 20 l reactor in inert condition. The reactor and the PFO were earlier purged with nitrogen. Mixing was adjusted to 400 rpm and temperature 20 °C.

20

Preparation of a EADC emulsion in PFO:

1.75 l (1.565 kg, 2.28 mol of Al) of EADC was then added to the reactor. If the PFO is pure from oxygen and moisture, there is no colour change in the EADC droplets. The EADC
25 solution forms an emulsion in PFO at 20 °C. To ensure full emulsification the mixture was mixed 400 rpm at 20 °C for 30 min.

Precipitation of MgCl_2 carrier:

3.31 l (2.44 kg, 2.24 mol of Mg) of a heptane solution of $\text{Mg}(-\text{O}-\text{CH}_2-\text{HC}(\text{C}_2\text{H}_5)-\text{C}_4\text{H}_9)_2$ (2.23 % Mg) was prepared by mixing BOMAG with heptane in the molar ratio of Mg:heptane of 1:6.65, adding 2-ethyl-hexanol slowly, at room temperature, in the molar ratio of Mg:ROH of 1:2, whereafter increasing the temperature of the mixture to 45 °C and mixing at this temperature for 30 min. The obtained solution was added during 45 min to the emulsion in the 20 l reactor. Already during the addition stage, the dispersion is changed from an emulsion to a suspension. After addition the temperature was increased to 70 °C. Mixing rate was 400 rpm. When the temperature of 70 °C was reached, the solution could optionally be held at this temperature for 30 min. Here after the reaction mixture was allowed to separate. Due to the high density of the PFO, the catalyst carrier floats on the surface of this solution. The PFO-hydrocarbon solution was separated from the carrier material by siphoning.

Hydrocarbon wash of the carrier:

9 l (6.6 kg, 66 mol) of heptane was added to the reactor. Mixing rate was 100 or 200 rpm and temperature 60 °C. The washing was continued for 20 min after which the carrier was allowed to settle for 20 - 30 min, depending on the experimental set up. The wash solution was drawn off by siphoning. Depending on the experiments this washing step was done just once or repeated twice, see above.

Preparation of the catalyst by addition of TiCl_4 :

7.1 l (5 kg, 30 mol) of heptane was added to the obtained support material to create a new slurry. Mixing rate was 200 rpm. Then 123 ml (212.2 g, 1.118 mol) of TiCl_4 was added to the reactor. The suspension was heated to 70 °C and the

reactants were allowed to react with each other for 45 min. After this the catalyst was allowed to settle for 20 min and the supernatant was then siphoned off. After this the catalyst was washed twice with heptane. The washing

5 procedures were the same as used when washing the carrier.

Take out of the catalyst:

2 l (1.37 kg, 13.7 mol) of heptane was added to the reactor to create a new suspension. This suspension was shifted over
10 to a receiving vessel.

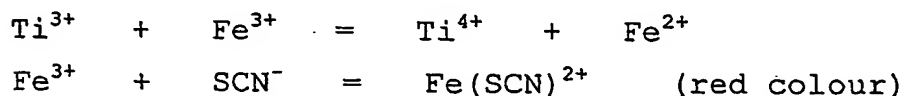
Determination of Ti, Mg and Al:

Samples were taken from the washed support material and from the catalyst.

15 The Al and Mg containing carrier samples and the Ti and Al containing catalyst samples were dissolved in a mixture of nitric and hydrofluoric acid and the metals were measured by flame atomic absorption with a nitrous oxide/acetylene flame. The results for the carrier material are listed in Table 2
20 and the results for the catalyst material are listed in Table 3.

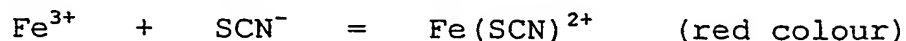
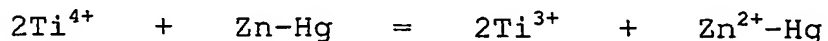
Determination of Ti^{4+} and Ti^{3+} :

For the determination of Ti^{3+} the sample is dissolved in
25 hydrochloric acid and Ti^{3+} is determined titrimetrically with a standard ferric sulphate solution with potassium thiocyanate as indicator (titration A):



30 For the determination of Ti^{4+} (titration B) a second sample is dissolved in hydrochloric acid and Ti^{4+} is reduced to Ti^{3+} by running the solution through a zinc amalgam reductor. Ti^{3+} is determined titrimetrically as in titration A. In this

titration the sum of Ti^{3+} and Ti^{4+} in the sample is determined. Ti^{4+} is obtained by subtracting the result from titration A from that of titration B:



The results are listed in Table 3.

PSD of carrier:

10 The particle size distribution of the carrier samples were done by known coulter measurements. From the coulter PSD curves the mode, i.e. the PS of the maximum fraction was measured. The results are listed in Table 2.

15 Test polymerisation:

A 3 l autoclave reactor was used. 1800 ml (1.127 kg, 15.6 mol) of pentane was introduced into the reactor as reaction medium. After adding the polymerisation medium the temperature of the reactor was adjusted to 90 °C. The co-catalyst and the catalyst were fed into the reactor by means of two feed vessels. TEA was used as co-catalyst. An Al/Ti molar ratio of 70 - 90 was used in the homo-polymerisations (about 0.5 ml TEA).

After introduction of the co-catalyst into the reactor, about 25 5 - 10 mg of the studied catalyst was fed together with 10 ml (6.3 g, 87 mmol) of pentane. An additional 500 ml feed vessel was connected to provide 17.5 bar of H_2 pressure (385 mmol). This amount corresponded to the so-called high MFR test polymerisation condition (see above). The polymerisation was 30 started by introducing both the H_2 together with the ethene monomer to the reactor. A total pressure of 14.4 bar was maintained by the ethene feed trough out the polymerisation. The polymerisation was carried out for 1 h at 90 °C. The

polymerisation was stopped by venting off the monomer and the pentane.

Characterisation of the polymers:

- 5 The polymers were characterised in respect of their particle size distribution. APS = average particle size. The results are listed in Table 4.

Table 2. Results of the support material

Example	1	2	3
Al/Mg molar ratio (mol/mol)	0.15	0.77	0.95
APS (μm)	13.6	16.4	18.0

10

Table 3. Results of the catalyst material

Example	1	2	3
Al/Ti molar ratio [mol/mol]	0.52	0.41	0.17
% as Ti^{2+}	21	22	34
% as Ti^{3+}	14	25	14
% as Ti^{4+}	65	53	52

Table 4. Results of the polymer material

Example	1	2	3
Activity, [kg PE/(g Ti h)]	239	319	165 ^{*)}
APS [mm]	0.22	0.31	0.38
Fines [%], d < 100 μm	13.8	11.1	4.4

*) Lower activity shows that increased PS and less fines are

15 not activity related

Example 4

The catalyst support and the final catalyst of the invention were prepared without the emulsion formation, i.e. using the starting material and conditions as described above in examples 1-3 of the invention, with the exception that no PFO was used and the wash hydrocarbon was changed from heptane to pentane. The polymerisation test was effected as described under "Test polymerisation" below. Activity was 241 kg PE/(g Ti h). Particle size of the carrier was 18.1 μm and particle size of the produced polymer was 0.45 mm showing 3.7 % of fines.

Comparative example

(as the closest prior with no recovery step of the support)

To show that a washing step is necessary after precipitation of the carrier material a comparative example was done on laboratory scale (5.1 mmol of Mg and Al). In this experiment the washing of the precipitated carrier material was left out, i.e. the titanation of the support material was carried out in the same solution as where the precipitation of the support had taken place. Otherwise the same conditions were used as in Example 4. The resulting polymer showed 6.2 % of very fine material and, in addition to that, > 50 % of fines material which was agglomerated to aggregates. About 15 % of the material had an irregular shape and had a diameter bigger than 2 mm.

The examples show the benefits of the loading of the carrier material of the invention and the effect of the washing step/no washing step on the content of the support material. It also appears that the mechanical strength of the carrier material of the invention is very good.